TRC 76

USE

OF

,

FLY ASH

IN

HIGHWAY CONSTRUCTION

TRC 76

FINAL REPORT OCTOBER 1986 USE

OF

FLY ASH

IN

HIGHWAY CONSTRUCTION

October 1986

by

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Conducted in cooperation with the U.S. Department of Transportation, Federal Highway Administration

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SUMMARY

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METRIC CONVERSION TABLE

| SYMBOL | KNOWN UNIT | MULTIPLY BY | TO FIND | SYMBOL |
|-----------------------|-------------------------------|---|--------------------------|--|
| | | LENGTH | | |
| in | inches | 2.54 | centimeters | CM |
| ft | feet | 30.48 | centimeters | C# |
| ft | feet | 0.30 | meters | m a state of the s |
| yd | yards | 0.91 | neters | m n |
| mì | miles | 1.61 | kilometers | km |
| 149 L | m1123 | | | |
| _ | | AREA | | - |
| in_2 | square inches | 6.45 | square cm | ະ ຕ ິ2 ເທີ2 |
| ft | square feet | 0.09 | square meter | 5 8 |
| in2 ft2 yd2 | square yards | 0.84 | square meter | ຣ ຄີ |
| ni Ai | square miles | 2.59 | sq. kilomete | rs km ² |
| | acres | 0.40 | hectares | ha |
| | acres | 4046.87 | square meter | ha s m |
| | | | | |
| . 3 | | VOLUME | | 3 |
| in3 ft3 | cubic inches | 16.39 | cubic cm | د ۾ع, دد |
| TT 3 | cubic feet | 0.03 | cubic meters | |
| ft ³ yd | cubic feet | 28317.0 | cubic cm cubic meters | cw2, cc |
| | cubic yards | 0.76 | | |
| gal | gallon (U.S.) | 3.79 | liter(1000 c | |
| qt | quart (U.S.) | 0.95 | liter | 3 |
| OZ (| ounce fluid) | 29.57 | cubic cm | cm ⁻ , cc |
| | | WEIGHT | | |
| 1Ь | pound(avoirdupo | | kilogram | kg |
| 16 | 94 69 | 453.59 | grams | g |
| oz | ounces(") | 28.35 | grams | g |
| | short ton(2000 l | b) 0.91 | tonnes(1000k | |
| | | | | |
| 15.5 | | FORCE, PRESSUR 4.45 | newtons | N |
| lbf | pounds-force | 4.40 | newcons | |
| nsi.lbf/ | in ² pound-force/s | nuare | | |
| p31,1017 | inch | 6.89 | kilopascals | kPa |
| | | | ···- | |
| f | oot of water(39.2 | °F) 2.99 | 56 | kPa |
| inch | of mercury(32 ⁰ F) | 3.39 | •• | kPa |
| - | | ANGLE | | |
| 0 | degrees | 0.017 _4 | radians | rad |
| • | minutes | 2.91x10 . | radians | rad |
| 84 | seconds | 4.85×10 ⁻⁶ | radians | rad |
| | | | | |
| | | TEMPERATURE | | |
| ⁰ F de | grees Fahrenheit | t ⁰ C=(t ⁰ F-32)/ | 1.8 degrees | Celcius ^O C |
| oc | degrees Celcius | ADD 273.15 | degrees Kelv | in ^O K |

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The Use of

Fly Ash in Highway Construction

Introduction

Fly ash is a powdery by-product of the coal combustion process, usually associated with electric power generating plants, and is recovered from flue gases. The chemistry of fly ash is such that in the presence of lime and moisture, pozzolanic properties are exhibited, i.e., cementitious products are produced which result in a material of increased strength and durability. These properties make some fly ashes suitable for use as a supplement or replacement for lime and/or portland cement in various construction materials.

Arkansas has available five sources of fly ash, each having its inherent chemical and physical composition. These sources include: White Bluff and Newark, owned and operated by Arkansas Power and Light Co.; Gentry and Casson, owned and operated by Gifford Hill Co.; and the Oklahoma Gas and Electric (OGE) plant.

As a result of several sources available and the increase in amount of pavement rehabilitation, the Arkansas Highway and Transportation Department initiated this research project in the summer of 1983 to study various combinations and percentages of fly ash and portland cement for pressure grouting mixes. This report summarizes the various materials and test results.

Materials

Pressure grout for pavement undersealing consists of fly ash, Portland Cement and water. The materials are blended together to

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obtain a flowable mixture which can be pumped through a 2 inch drill hole in the concrete pavement to voids below the pavement.

The following paragraphs will summarize the source of each material.

Water

Water used shall be clean, potable and free from injurious amounts of oil, salts or other deleterious substances. The water used for this project met all applicable requirements of Section 501 of the Arkansas State Highway and Transportation Department's 1978 Standard Specifications for Highway Construction and was obtained from the City of Little Rock's Water Supply System.

Portland Cement

Portland Cement was obtained from two sources which are most commonly used and readily available within the State of Arkansas. Both sources meet the applicable requirements of Section 501 of the Standard Specifications.

Ideal cement was obtained from Ideal Cement Company in Okay, Arkansas. The results of physical and chemical tests of a typical sample of Ideal cement are shown in Figure 1. This sample complied with AASHTO Specification M85 for Type I Portland cement.

Foremen cement was obtained from Arkansas Cement Corporation at Foreman, Arkansas. The results of physical and chemical tests of a typical sample of Foreman Cement are shown in Figure 2. This sample complied with AASHTO Specification M85 for Type I Portland cement.

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Fly Ash

Fly ash was obtained from five separate sources which are available to Arkansas. All five sources met ASTM C618 Class "C" fly ash specifications. The fly ash sources used and locations are as follows:

White Bluff fly ash is produced at the Arkansas Power and Light's coal fired generating plant at White Bluff near Redfield, Arkansas.

Newark fly ash is produced at the Arkansas Power and Light's coal fired generating plant at Newark near Newport, Arkansas.

Gentry fly ash is produced at the Gifford Hill coal fired generating plant at Gentry, Arkansas.

OGE fly ash is produced at the Oklahoma Gas and Electric coal fired generating plant at Muskogee, Oklahoma.

Casson fly ash is produced at the Gifford Hill coal fired generating plant at Casson, Texas.

Initial Investigation

In 1982 and 1983, when this project was initiated, very little pavement undersealing was being performed in Arkansas with the exception of district maintenance work. Therefore, an investigation was performed to determine what materials were being used and the blends of each material, from all ten districts. The Districts that performed undersealing operations used a sandy-silty native soil and cement at the following proportions:

| Di | st: | ri | ct |
|----|-----|----|----|
| | | | |

Mix

| 1 | 0.5 | bags | cement | $/yd^3$ | soil |
|----|---------|--------|--------|------------------|------|
| 2 | 1.5-2.0 | " | F1 | - 1 | 11 |
| 3 | 7.0 | " | 17 | " | |
| 4 | 3.0 | | ** | " | н |
| 5 | 3.0-4.0 | 11 | ** | ** | 89 |
| 6 | 1.0 | " | | | 11 |
| 7 | 2.0-3.0 | " | 88 | H | ** |
| 8 | 1.8 | ** | " | 11 | 11 |
| 9 | No c | operat | tion | | |
| 10 | 4.0 | bags | cement | /yd ³ | soil |

Unconfined compressive strength samples were molded with various mixtures of cement, fly ash and native soil. The results of these tests are shown in Table 1. The 7-day compressive strengths ranged from 16 psi for 3 bags fly ash : 2 bags Portland cement : 1 yard of sand to 104 psi for 3 bags Portland cement : 1 yard sand.

From the results of these initial tests and an article published in Transportation Research Record (TRR) No. 800, a testing program was established for all pressure grouting jobs.

Testing Program

A testing program was established to determine criteria for a pressure grouting mixture. The tests included flow cone, set times, compressive strengths, and durability testing. From the results of TRR No. 800 and information from other State Highway Departments, testing was performed on various mixtures of fly ash, Portland cement, admixtures, and water.

Mixture

The various mixtures of fly ash and Portland cement consisted of 2:1, 3:1, 3.5:1 and 4:1 parts of fly ash to parts of Portland

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| Ratio Agent(s)/Soil FA=Fly Ash PC=Portland Cement YS=Cu.Yard Soil | 7 Day Compressive Strengths 4" Dia. Spec. 4-Hour Soak | 7 Day Vacuum Sat.Strengths 4" Diameter Specimens | Wet-Dry Durability Approx.&Loss/ Cycles | Freeze-Thaw Durability Approximate %Loss/Cycles | Cube Strength Dry Cure PSI/days cure | Cube Strength Wet Cure PSI/days cure | Rating In Relation to Other Mixtures |
|---|---|--|--|--|---|---|---|
| l FA 1 YS | Dissolved in Soak | ĸ | 100%/0 cycles | 100%/0 cycles 0/1 7/2 0/5 | 0/1 7/2 0/5 | 0/1 0/2 0/5 | Poor |
| 2 FA 2 PC 1 YS | 29 | 27 | Sample Broke Apart No Test | 66% ê5 cycles | 43/1 64/4 55/5 | 17/1 23/4 19/5 | Poor |
| 3 FA 1 PC 1 YS | 1 6 | 15 | 100%/0 cycles | 100%/3 cycles | No sample | No sample | Poor |
| 1 FA 1 PC 1 YS | 115 | 67 | 20%/12 cycles | 15%/12 cycles | 70/1 87/2 71/5 | 24/1 41/2 57/3 | Fair |
| 5½ FAIPC ½ YS L | • • • | 35 | 60%/10 cycles | 35%/12 cycles | 44/1 44/2 45/5 | 14/1 17/2 19/5 | Poor |
| T 4 PC 1 YS | 50 | 56 | 50%/3 cycles | 50%/5 cycles | 11/1 32/4 24/5 | 1/1 3/4 5/5 | Poor |
| 2 PC 1 YS | 68 | 83 | 35%/12 cycles | 15%/12 cycles | 30/1 61/2 76/3 | 71/1 102/2 101/3 | Fair |
| 3 PC 1 YS | 104 | 103 | 5%/12 cycles | 15%/12 cycles | 12/1 23/2 35/3 | 23/1 43/2 59/3 Fair (Best Overall) | Fair 2rall) |
| 1 PC 1 YS | 43 | 44 | Broke Apart/ 1 cycle | 30%/7 cycles | 31/1 49/2 49/3 | 11/1 17/2 22/3 | Poor |
| 7 PC 1 YS | 44 | 43 | 35%/6 cycles | 85%/8 cycles | 66/1 76/2 58/5 | 22/1 37/2 62/5 Poor | Poor |
| | | | | | | | |

Table 1: LABORATORY RESULTS OF MAINTENANCE MIXES

One 6" Diameter Cylinder - 12" long - was tested for mixture - 1 PC 1 YS Molded 4/13/82. Tested 10/26/82. Approximately 6 months = 175 psi - dry cured.

cement. Each batch consisted of 12,000 grams dry weight of solids. The proper proportions of fly ash and Portland cement were thoroughly mixed before adding water.

The required amount of water to produce a time of efflux of 10 to 25 seconds was poured into a 5-gallon plastic bucket, then the pre-mixed fly ash and Portland cement were added in three increments. A hand-held electric drill with a paint mixing attachment was used to continuously mix the sample as the fly ash and cement were being added. After the last increment was added, the sample was mixed for 3 minutes. Immediately after mixing, a temperature was taken and three consecutive flow cone readings were performed. The average of the three readings was specified to be between 10 and 25 seconds. Once the flow has been adjusted properly the sample is molded into 4 in. x 5 in. specimens for 24 hr., 4-Day and 7-Day compressive strengths and set times.

Durability samples were also molded on a few samples but were later suspended due to the difficulty that all of the moisture could not be extracted from the specimens to determine an accurate percentage wear loss.

Testing Procedures

Compressive Strengths

A total of 27 specimens were molded for 24 hour, 4-day and 7-day compressive strengths. Three specimens from each time group were cured at the following temperatures: Moisture Closet $(72^{\circ}F)$, Refrigerator $(45^{\circ}F)$, and variable outside temperatures located on dock of Materials and Research laboratory.

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Set Times

Two types of set times were performed on each mixture and curing condition. One method was the Gilmore Needle (AASHTO T-154) which consists of a small sample which was cured under the previous stated conditions. A needle was used to penetrate into the sample at various times until there was no penetration. The time was then recorded for set. The second method, developed for this project, determined the temperature and consistency of the interior of the specimen.

Test Results

The results of all tests are shown in Table 2. The set times ranged from 20 hours to 70 hours depending on the mix and curing conditions. The compressive strengths were higher for specimens cured in the moisture closet. Each compressive strength shown in Table 2 is an average of three specimens. The specimens cured in the refrigerator and on the dock were considerably weaker than the specimens cured in the moisture closet.

Additives

Various air entraining agents or water reducers were used with a 3 part fly ash to 1 part Portland cement mixture to determine their effects on the mixture. Additives that were used include 344N, WRDA-19, and LL.

The additives were added to the mix water before the solids were introduced. The results of these tests are shown in Table 2. As set time decreased, the 7-day compressive strengths also decreased. As a result of these tests, further testing with additives was suspended.

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| Comments | No Measurement | No Measurement | Discontinued FT at 7 cycles-falling apart | No Measurement | Discontinued FT at . 6 cycles-falling apart | Note the swell | · | | First time weighed. Lifted small weight & plastic cover & swelled | at bottom Plastic Plates & approx. 50# Wt. | | | Note the shrink | High shrink | | |
|--|-------------------------------------|--|--|--|--|---|--|--|---|--|---|--|-------------------------|---|---|---------------------------------------|
| <u>shrink</u> <u>Swell</u> Avg. (Inches) | 0.05 Est/NM | MN/MN | 0.05 Est/0.0 | MRVMN | 0.05/0.0 | 0.0/0.34 | 00°0/11N | 0.0/0.16 | 0.0/0.15W* | .05/W | W/00. | W/00. | .03/W | W/II. | .01/W | |
| 28 Day Compressive Strengths (psi) | No sample | No sample | No sample | No sample | No sample | 485 | 2189 | 199 | 1025 | 4405 | 6008 | 6923 | 5909 | | | |
| 7 Day Compressive Strengths Avg. (psi) | 1540 | 120 | 484 | 180 | 1826 | 62 | 400 | 163 | 88 | 1659 | 333 | 497 | 1293 | 298 | 1225 | 616 |
| Times Cured Initial/Final (Minutes) | 95/235 | 107/157 | 215/255 | 158/176 | 205/270 | 162/300 | 135/180 | 187/225 | 155/225 | 175/405 | 210/280 | 167/295 | 165/265 | Estimated 375/555 | 123/218 | Estimated |
| Set Times Moist Cured Initial/Final (Minutes) | No sample | 137/182 | 185/225 | 162/182 | 345/1515 | 180/340 | 140/185 | 190/230 | 162/375 | 435/1345 | 240/310 | 240/330 | 230/340 | Estimated 495/675 | 158/278 | Estimated |
| Flow Cone S Avg. of 3 M (Sec.) 1 | 13.2 | 10.9 | 12.1 | 12.0 | 16.1 | 11.2 | 11.5 | 12.2 | 1.11 | 14.2 | 13.9 | 17.7 | 15.3 | 10.2 | 14.7 | 13.7 |
| Tenperatures of Room/Water/Mix | 2T/0T/2T | 76/74/73 | 74/68/70 | 74/75/74 | 11/12/11 | 72/73/70 | 13/13/10 | 70/73/69 | 74/70/70 | 72/75/72 | 15/71/71 | 11/13/11 | 75/72/72 | . 72/75/71 | 73/74/72 | 74/74/74 |
| Date Mixed all 3 Minutes | 1/5/84 | 1/6/84 | 1/9/84 | 1/10/84 | 1/11/84 | 1/12/84 | 1/13/84 | 1/16/84 | 1/25/84 | 1/26/84 | 1/27/84 | 1/30/84 | 1/31/84 | 2/7/84 | 2/8/84 | 2/16/84 |
| Blend No composition | B-1 3FA:1PC 338 H ₂ O | B-2 3FA:1PC 1%LL 33% H ₂ O | B-3 3FA:1PC 0.1% 344N 33% H ₂ O | B-4 3FA:1PC 1% LL 0.4% 33% H ₂ O 344N | B-5 3FA:1PC 328 H20 | B-6 3FA: IPC 18LL 328 H ₂ O | B-7 3FA:1PC 0.4% 344N 32% H ₂ O | B-8 3FA:1PC 1%LL 0.4% 344N 31% H ₂ O | B-9 3FA: IPC 1811 328 H20 | B-10 3FA:1PC .073%LI 32% H ₂ O | B-11 3FA:1PC .25%LL 30% H ₂ O | B-12 3FA:1PC 15%LL 29% H ₂ O | B-13 3FA:1PC 32% H2O | B-14 3FA: IPC 33% H2O 0.85% WRDA-19 | B-15 .3FA:1PC 29% H>O 0.24% WRDA-19 | B-16 3FA:1PC 30% H2O 0.25% 344N |

Table 2: FREEZE/THAW VACUUM/SPIURATION RESULTS

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Conclusions

- In all mixtures the 7-day compressive strengths of 3:1 and
 3.5:1 produce higher strengths.
- 2. The set times were much longer for samples cured in the refrigerator and on the dock than in the moisture closet.
- Additives used to help reduce set times during colder weather were successful, but they also drastically reduced the 7-day compressive strengths.
- 4. Curing temperature under the pavement slab is a major factor that affects grout mixture performance.

Recommendations

On the basis of the limitations of the test procedures and for the range of materials and conditions utilized in this investigation, the following recommendations are warranted:

- Submit proper amounts of fly ash and Portland cement to the Materials and Research Laboratories for a pressure grout design.
- Grouting of concrete pavements with slab temperature below 55^oF should not be allowed.
- 3. Specify a minimum of 4 days for proper curing of the grout.

